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Maintenance and Decision Tools

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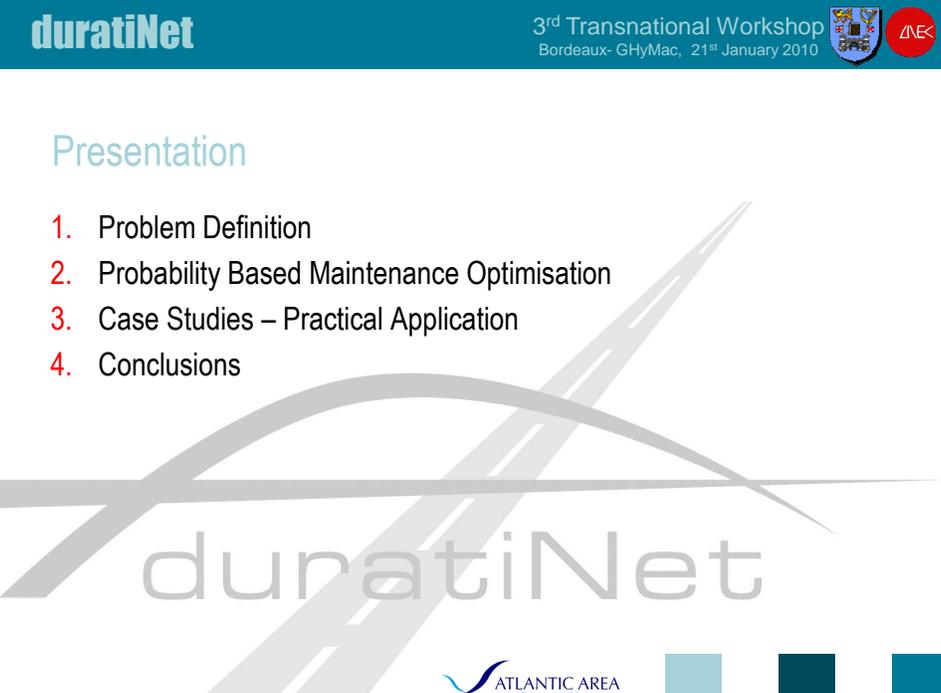
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Bordeaux- GHyMac, 21st January 2010

Presentation

1. Problem Definition
2. Probability Based Maintenance Optimisation
3. Case Studies – Practical Application
4. Conclusions



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1. Problem Definition

A common problem among bridge owners/managers is the need to reduce spending whilst attempting to operate and maintain an increasingly ageing bridge stock which is subject to a loading intensity for which, in many cases, it was not designed.



That structures have lived shorter than their design life!



Tianjin, China, 15 July 2009



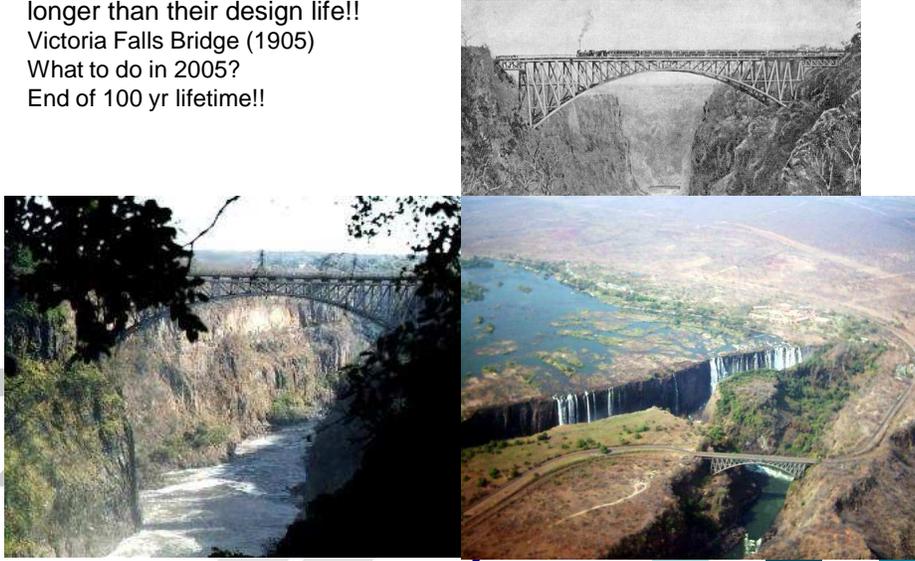
Ireland, 21 August 2009



Zuzhou flyover,
China, 17 May 2009

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Or that structures have lived longer than their design life!!
Victoria Falls Bridge (1905)
What to do in 2005?
End of 100 yr lifetime!!





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1. Problem Definition

For a given structure how do we decide upon the optimal maintenance strategy as a function of age, condition, importance, **required remaining life** etc. in a robust/repeatable manner, avoiding generalisation/excessive conservatism such that our maintenance budget is optimised???

e.g. Storstrom 1937, 3.2km






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Question 1:

- Does a bridge necessarily have to fulfill the specific requirement of the general code as long as the overall requirement for the safety is satisfied.

The graph plots Safety level on the y-axis against Age on the x-axis. A solid curve represents the bridge's condition over time, starting at an "Optimal" condition and declining. A horizontal line indicates the "Minimum safety level" with a reliability index $\beta > 4.75$. Three maintenance actions are indicated by dashed lines: "A Do Nothing" at the lowest point, "B Cathodic Protection" at a slightly higher point, and "C Extensive repair" at a higher point. An inset photo shows a bridge deck with extensive repair work. A smaller inset photo shows a bridge deck with cathodic protection. A graph of $R(t)$ and $S(t)$ is shown in the bottom left. A vector $u = (\epsilon, z, A, \theta)$ is shown in the top right.

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Question 2:

- Does a bridge necessarily have to be pretty to be safe?

The photograph shows the underside of a concrete bridge. There is significant damage to the concrete, including large areas of spalling and exposed, rusted reinforcement bars. The support columns also show signs of corrosion and staining. The bridge is situated over a body of water, and a green safety net is visible in the background.

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2. Probability Based Maintenance Optimisation

Statistical Modelling of:

- Loads
- Resistances
- Uncertainties

Updating based upon results of tests/inspections

Purpose:
Cut strengthening or rehabilitation costs without compromising the safety level

Table 1 – Minimum Safety Levels Specified by the Eurocode (EN1990:2002)

Reliability Class	Minimum values for β	
	1 year reference period	50 year reference period
CC3 (RC3)	5.2	4.3
CC2 (RC2)	4.7	3.8
CC1 (RC1)	4.2	3.3

Essentially a Bridge specific "code" is obtained

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2. Probability Based Maintenance Optimisation

Legal Basis – Eurocode 1 Basis of Design

Safety Level NEVER Compromised – Rather Optimised

EUROPEAN STANDARD EN 1990
NORME EUROPÉENNE
EUROPAISCHE NORM

April 2002

CEN

European Committee for Standardization

Comité Européen de Normalisation

Europäischer Ausschuss für Normung

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3.5 Limit state design

(1) Design for limit states shall be based on the use of structural and load models for relevant limit states.

(2) It shall be verified that no limit state is exceeded when relevant design values for – actions, – material properties, or – product properties, and – geometrical data are used in these models.

(3) The verifications shall be carried out for all relevant design situations and load cases.

(4) The requirements of 3.5(1)P should be achieved by the partial factor method, described in section 6.

(5) As an alternative, a design directly based on probabilistic methods may be used.

NOTE 1 The relevant authority can give specific conditions for use.

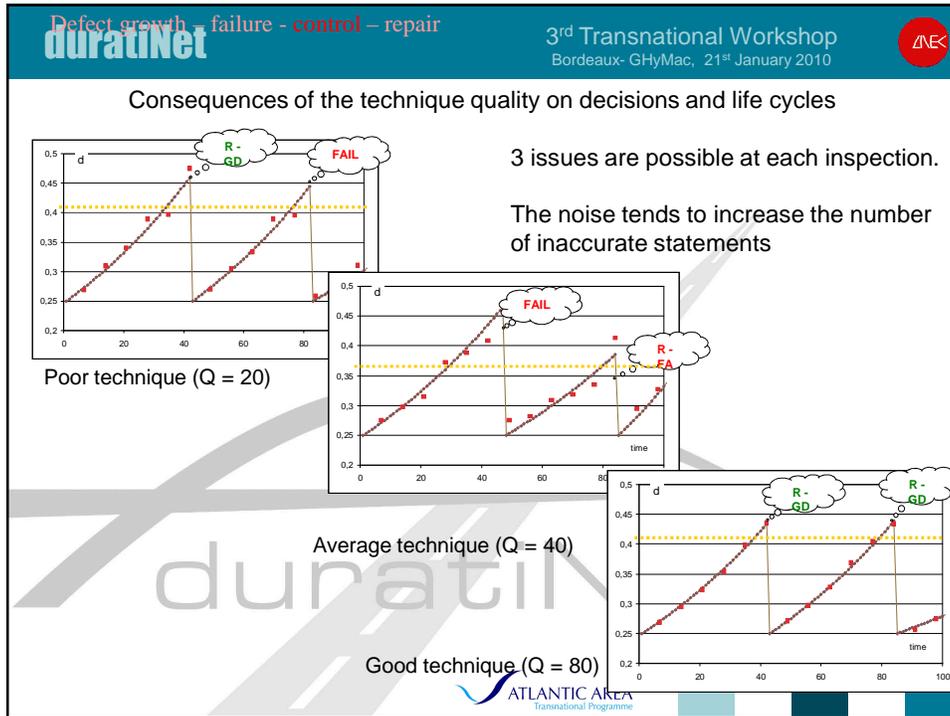
NOTE 2 For a basis of probabilistic methods, see Annex C.

(6) The selected design situations shall be considered and critical load cases identified.

(7) For a particular verification load cases should be selected, identifying compatible load arrangements, sets of deformations and imperfections that should be considered simultaneously with fixed variable actions and permanent actions.

(8) Possible deviations from the assumed directions or positions of actions shall be taken into account.

(9) Structural and load models can be either physical models or mathematical models.



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3. Case Studies

(i) Storstrom Bridge

- The 3.2 km long Storstrom Bridge connects the Danish Island of Zealand with the southern Danish islands of Falster and Lolland.
- The bridge opened in September 1937.



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Storstrom Bridge: Results of Assessment

Deterministic assessment of the deck slab using PROCON for combined dead and live load produced a **maximum load factor of 0.61**. This implies that the slab is incapable of sustaining the applied load. The recommendation would therefore involve costly rehabilitation of the structure.

Probabilistic Assessment including deterioration modelling, **with deterioration models updated based upon inspection** results performed at the bridge could document sufficient capacity.

Table 5 - Results of deterministic and probabilistic assessment; O'Connor et al (2004).

Load Combination	Self Weight + KL10 Live Load
Deterministic plastic load carrying capacity	61 %
Probabilistic Assessment: No deterioration	$p_f = 2.94 \times 10^{-13}$ $\beta = 7.20$
Probabilistic Assessment: Stochastic modelling of deterioration according to inspections results	$p_f = 6.92 \times 10^{-7}$ $\beta = 4.83$

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Over side: Mere end 60 cm fra fluge (3.0 cm)
20-60 cm fra fluge (2.5 cm) | 0-30 cm fra fluge (1.5 cm)
Fluge
Under side: 20-60 cm fra fluge (2.5 cm) | 0-20 cm fra fluge (0.5 cm)
Mere end 60 cm fra fluge (3.5 cm)

	Område A (0 S. msh)	Område B (0 S. kant)	Område C (11 S. msh)	Område D (11 S. kant)
Langsgående: 0-30 cm 0-20 cm	N(91.16)	N(74.20)	N(91.16)	N(73.14)
30-60 cm 20-60 cm	N(95.6)	N(95.6)	N(95.6)	N(85.17)
Større end 60 cm	N(95.6)	N(95.6)	N(95.6)	N(95.6)
Tværgående: 0-30 cm 0-20 cm	N(95.6)	N(86.12)	N(95.6)	N(85.14)
30-60 cm 20-60 cm	N(95.6)	N(95.6)	N(95.6)	N(95.6)
Større end 60 cm	N(95.6)	N(95.6)	N(95.6)	N(95.6)

Tabel 7-3 Bestemte stokastisk modeller af armeringens tværsnitareal i år 2002.

Computed beta for cases considered

Case	Year	beta
(1) Case 1	2002	7.00
(2) Case 2	2007	6.58
(3) Case 3	2017	5.65
(4) Case 4	2005	6.70
(5) Case 5	2007 (20% ModUnc)	5.73
(6) Case 6	2017 (20% ModUnc)	4.65
(7) Case 7	2007 (Reduced Cover)	5.99
(8) Case 8	2017 (Reduced Cover)	4.86

Legend: Case 1 (blue), Case 2 (red), Case 3 (green), Case 4 (purple), Case 5 (orange), Case 6 (brown), Case 7 (pink), Case 8 (grey)

Updating of parameters through e.g. inspection results can reduce uncertainty and improve β , or vice versa (i.e. Intelligent Assessment, Structural Health Monitoring)

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(ii) Bergeforsen Railway Bridge, Sweden

Bridge constructed in 1923
Superstructure span configuration: 42+84+42 = 168m
Side spans 22.5m + 11.6m
Total bridge length = 202.1m
Required to assess for **Heavier Trains**

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Structural analysis was performed using an FE model calibrated against a shell and volume element model constructed for specific critical locations.

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Deterministic assessment - results

• SLS capacity demo
• FLS capacity demo
• ULS capacity could be performed at these critical locations

Figur 6-1 Opstait af DIP55-profilier.

(a) Connection 2-D₂

Model UB: ULS: Udnyttelsestrader TB General

Location	ULS Capacity (Ratio)
1 (syd)	0.80
2 (syd)	0.80
3 (syd)	0.90
4 (syd)	1.10
5 (syd)	1.15
6 (syd)	1.15
7 (syd)	1.15
8 (syd)	1.15
9 (syd)	1.15
10 (syd)	1.15
11 (syd)	1.15
12 (syd)	1.15
13 (mitte)	1.15
12 (nord)	1.15
11 (nord)	1.15
10 (nord)	1.15
9 (nord)	1.15
8 (nord)	1.15
7 (nord)	1.15
6 (nord)	1.15
5 (nord)	1.15
4 (nord)	1.15
3 (nord)	1.15
2 (nord)	1.15
1 (nord)	1.15

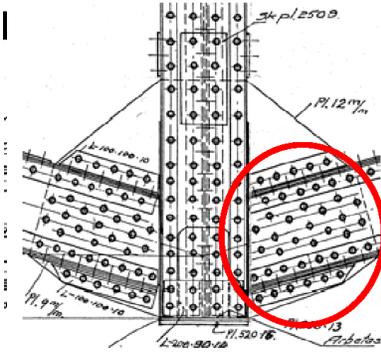
Concluded that probability based assessment should be performed at these critical locations.

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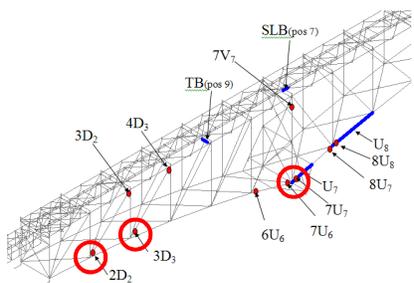


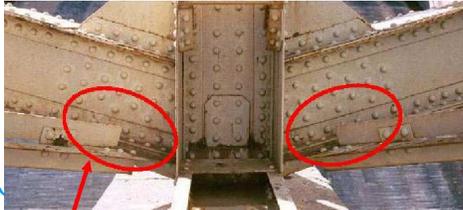
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(a) Connection 7-U₇

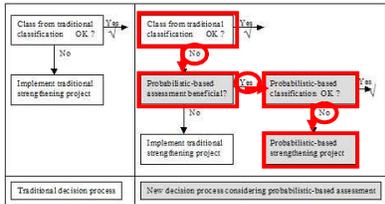


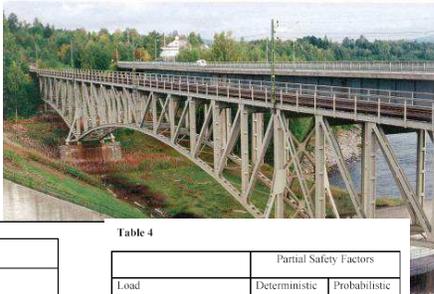




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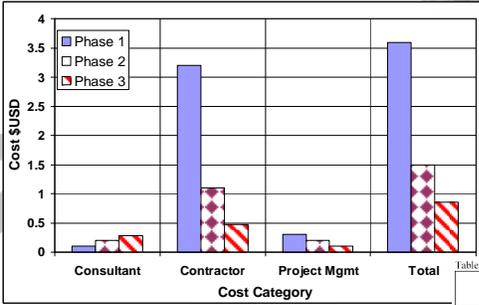


Table 4

Load	Partial Safety Factors	
	Deterministic	Probabilistic
Dead Load	1.0	1.03
Superimposed Dead Load	1.0	1.02
Train Load Global	1.3	1.21
Train Load Local	1.3	1.20
Dynamic Factor Global	1.08	1.05
Dynamic Factor Local	1.47	1.32

Table 7 - Results of deterministic and probabilistic assessment; O'Connor et al. (2004).

	Phase 1 Deterministic Assessment (\$USD)	Phase 2 Advanced Deterministic Assessment (\$USD)	Phase 3 Probability Based Assessment (\$USD)
Consultant Fee	\$0.1ml	\$0.2ml	\$0.28ml
Contractor Fee	\$3.2ml	\$1.1ml	\$0.47ml
Project Management	\$0.3ml	\$0.2ml	\$0.1ml
Total Cost	\$3.6ml	\$1.5ml	\$0.85ml



4. Conclusion

- Case studies are presented to demonstrate to practical application of probability based approaches in optimal maintenance planning for existing bridges.
- In **NO** way has the safety of the structure been compromised rather a bridge specific code has been derived.
- The justification for the application of probability-based methods to bridges is provided from national codes and the Eurocodes.
- There are no practical or technical obstacles in applying probability-based techniques.
- A clear advantage of the approach lies in its ability to incorporate **bridge specific information and bridge specific safety modelling.**
- Applying the probability-based approaches **can result in considerable monetary savings by optimising maintenance strategies** for existing bridges.

